

Improved fits for  $E_1(x)$  *vis-à-vis* those presented in ARL-TR-1758

Efforts were made since the publication of ARL-TR-1758[1] to improve upon the accuracy of the fits presented in that document. Using the terminology of that report, the fit is actually done on  $F_1(w)$ , where  $w = 1/x$  and the function  $F_1 = E_1 e^{1/w}/w$  (*i.e.*,  $F_1 = x e^x E_1$ ). This transformation provides for a function  $F_1(w)$  which varies smoothly from unity (at  $w = 0$ ) to zero (as  $w \rightarrow \infty$ ). The fits were developed to minimize the largest occurrence of the error function  $\epsilon = [(F_1)_{\text{fit}} - F_1]/F_1$  at any point on the functional domain ( $0 \leq w < \infty$ ).

Several fits were developed, with greater accuracy resulting from the use of more parameters. In all cases, the fitted value of  $F_1$  takes the form

$$(F_1)_{\text{fit}} = 1/w \cdot \ln \{1 + w - [w - \ln(1 + w)] \cdot f(w)\} \quad . \quad (1)$$

Different fitting forms for  $f$  are presented below, with the associated values of  $\max(\epsilon)$  and the value of  $w$  for which the  $\max(\epsilon)$  occurs.

#### 6-Parameter Fit:

$$f(w) = \frac{1 + Aw + (1 - e^{-\gamma})Bw^2}{1 + \left(A + \frac{5}{3}\right)w \frac{1 + C_1 w^2}{1 + D_1 w^2} + Bw^2 \frac{C_2 + w^2}{D_2 + w^2}} \quad , \quad (2)$$

where

$$\begin{aligned} A &= 4.69041102625857590\text{D}+00 \\ B &= 7.76097664114015200\text{D}+00 \\ C_1 &= 2.30659438867190370\text{D}-01 \\ D_1 &= 2.37827207448962350\text{D}-01 \\ C_2 &= 1.40614716699937220\text{D}+02 \\ D_2 &= 1.39838508752857140\text{D}+02 \end{aligned}$$

$$\max(\epsilon) = 1.709092\text{E}-05 \text{ at } w = 99.782947.$$

**8-Parameter Fit:**

$$f(w) = \frac{1 + Aw + (1 - e^{-\gamma})Bw^2}{1 + \left(A + \frac{5}{3}\right)w + Bw^2 \left(1 + \frac{C_1}{D_1 + w} + \frac{C_2 w}{(D_2 + w)^2} + \frac{C_3 w^2}{(D_3 + w)^3}\right)} \quad , \quad (3)$$

where

$$\begin{aligned} A &= 4.99191263403800090\text{D}+00 \\ B &= 8.55392302479002180\text{D}+00 \\ C_1 &= 2.41723456633978670\text{D}+00 \\ D_1 &= 3.38951420119681250\text{D}+02 \\ C_2 &= -1.22812127267525170\text{D}+00 \\ D_2 &= 1.37651629589202030\text{D}+02 \\ C_3 &= -5.35044576792352150\text{D}-02 \\ D_3 &= 8.67574715486645330\text{D}-01 \end{aligned}$$

$$\max(\epsilon) = 3.256059\text{E}-06 \text{ at } w = 14.116516.$$

**10-Parameter Fit:**

$$f(w) = \frac{1 + Aw + B(1 - e^{-\gamma})w^2}{1 + \left(A + \frac{5}{3}\right)w \frac{1 + E_1 w^2 + C_1 w^3}{1 + G_1 w^2 + D_1 w^3} + Bw^2 \frac{C_2 + E_2 w + w^2}{D_2 + G_2 w + w^2}} \quad , \quad (4)$$

where

$$\begin{aligned} A &= 7.74823271875959920\text{D}+00 \\ B &= 2.42331702915707580\text{D}+01 \\ C_1 &= 3.48159341103108960\text{D}-03 \\ D_1 &= 1.01421240602993130\text{D}-03 \\ C_2 &= 7.77813337451483160\text{D}+01 \\ D_2 &= 9.41171735762913930\text{D}+01 \\ E_1 &= 9.52872674659433150\text{D}-01 \\ G_1 &= 9.43128313648529780\text{D}-01 \\ E_2 &= 6.29952753733901360\text{D}+01 \\ G_2 &= 6.28722150790988370\text{D}+01 \end{aligned}$$

$$\max(\epsilon) = 1.882788\text{E}-06 \text{ at } w = 45.275091.$$

### 12-Parameter Fit:

$$f(w) = \frac{1 + Aw + B(1 - e^{-\gamma})w^2}{1 + \frac{A + 5/3 + H_1 w}{1 + H_2 w} w \frac{1 + E_1 w^2 + C_1 w^3}{1 + G_1 w^2 + D_1 w^3} + B w^2 \frac{C_2 + E_2 w + w^2}{D_2 + G_2 w + w^2}} \quad , \quad (5)$$

where

$A = 6.58272149564893640\text{D}+00$   
 $B = 1.65978816181933130\text{D}+01$   
 $C_1 = 5.14357696611253590\text{D}-03$   
 $D_1 = 2.33075091216811960\text{D}-03$   
 $C_2 = 7.13737271086793040\text{D}+01$   
 $D_2 = 8.03410183545183260\text{D}+01$   
 $E_1 = 7.58135938490494650\text{D}-01$   
 $G_1 = 7.56175417133594260\text{D}-01$   
 $E_2 = 4.63752805419194370\text{D}+01$   
 $G_2 = 4.63079462234788510\text{D}+01$   
 $H_1 = 2.97036738105914930\text{D}-03$   
 $H_2 = 1.92452599275716720\text{D}-04$

$\max(\epsilon) = 3.076770\text{E}-07$  at  $w = 0.072472$ .

## References

1. S. B. Segletes. A compact analytical fit to the exponential integral  $E_1(x)$ . Technical Report ARL-TR-1758, U.S. Army Ballistic Research Laboratory, Aberdeen Proving Ground, MD, September 1998.

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